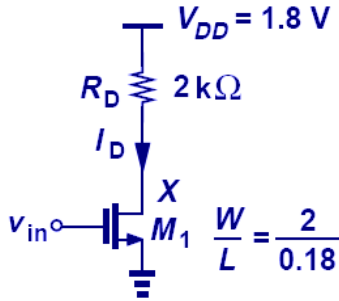


Name:

ID#

1. (8%) Calculate the small signal voltage gain of the CS stage if  $I_D=1mA$ ,  $\mu_n C_{ox}=100\mu A/V^2$ , and  $V_{TH}=0.5V$  and  $\lambda=0$ . Verify that  $M_1$  is in the saturation.  $g_m = \sqrt{2\mu_n C_{ox} \frac{W}{L} I_D}$



Ans:

$$R_D I_D < V_{DD} - (V_{GS} - V_{TH})$$

$$g_m = \sqrt{2\mu_n C_{ox} \frac{W}{L} I_D} = \sqrt{2 \times 100\mu \times \frac{2}{0.18} \times 1m} = \frac{1}{670.82\Omega}$$

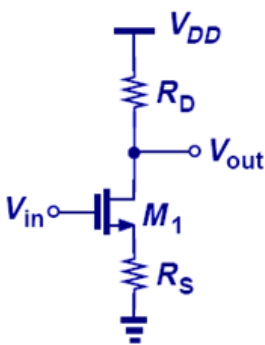
$$A_v = -g_m R_D = -\frac{1}{670.82} 2k = -2.98$$

$$V_{GS} = V_{TH} + \sqrt{\frac{2I_D}{\mu_n C_{ox} \frac{W}{L}}} = 0.5 + \sqrt{\frac{2 \times 1m}{100\mu \times \frac{2}{0.18}}} = 1.84V$$

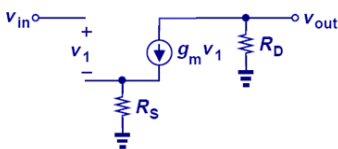
$$V_{DD} - R_D I_D = 1.8 - 2k \times 1mA = 1.6V \quad V_{GS} - V_{TH} = 1.84 - 0.5 = 1.34$$

the device is saturation and has a margin of 0.26V with respect to the triode region

2. (6%) Draw the small signal model of the following source degeneration circuit. And find the small signal gain of the following circuit.



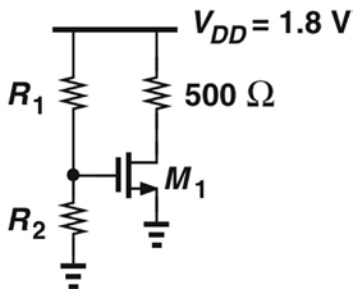
Ans:



$$v_{in} = v_1 + g_m v_1 R_S \Rightarrow v_1 = \frac{v_{in}}{1 + g_m R_S} \quad v_{out} = -g_m v_1 R_D \quad \frac{v_{out}}{v_{in}} = -\frac{g_m R_D}{1 + g_m R_S} = -\frac{R_D}{\frac{1}{g_m} + R_S}$$

3. (12%) For  $I_D=1\text{mA}$  and  $W/L=20/0.18$ . compute  $R_1$  and  $R_2$  such that input impedance at least  $20\text{k}\Omega$ .

$$\mu_n C_{ox}=200\mu\text{A}/\text{V}^2, \text{ and } V_{TH}=0.5\text{V} \text{ and } \lambda=0. \quad I_D = \frac{1}{2} \mu_n C_{ox} \frac{W}{L} (V_{GS} - V_{TH})^2$$



Ans:

② To get  $I_{DS} = 1\text{mA}$ ,

$$\frac{1}{2} \mu C_{ox} \left(\frac{W}{L}\right) (V_{GS} - V_{TH})^2 = 1 \times 10^{-3} \text{ A.}$$

$$\frac{1}{2} (200 \times 10^{-6}) \left(\frac{20}{0.18}\right) (V_{GS} - V_{TH})^2 = 10^{-3}$$

$$(V_{GS} - V_{TH})^2 = 0.09$$

$$V_{GS} - V_{TH} = 0.3,$$

$$\text{ie. } V_{GS} = 0.7.,$$

Since  $V_{GS} = \frac{R_2}{R_1 + R_2} \times 1.8$

$$0.7 = \frac{R_2}{R_1 + R_2} \times 1.8$$

$$0.7 R_1 = R_2,$$

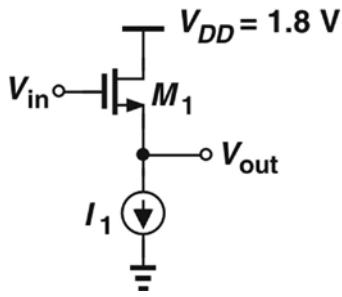
$$\therefore \frac{R_1}{R_2} = \frac{11}{7}. \quad \text{————— (1)}$$

To get input impedance  $\geq 20\text{k}$ .

$$R_1 // R_2 \geq 20\text{k}\Omega. \quad \text{————— (2)}$$

By inspection, setting  $R_1 = 55\text{k}\Omega$  and  $R_2 = 35\text{k}\Omega$  will satisfy both (1) and (2).

4. (8%) The circuit exhibits an output impedance of less than  $50\Omega$  with a power budget of  $2\text{mW}$ . Determine the  $W/L$ . Assume  $\lambda=0$ ,  $\mu_n C_{ox}=200\mu\text{A}/\text{V}^2$ , and the output impedance seen at  $M_1$  is only  $1/g_{m1}$ .



$$g_m = \sqrt{2\mu_n C_{ox} \frac{W}{L} I_D}$$

Ans:

(53). To see  $R_{out} = 50\Omega$ ,

$$\frac{1}{g_m} = 50\Omega$$

$$\therefore g_m = 20\text{mS}$$

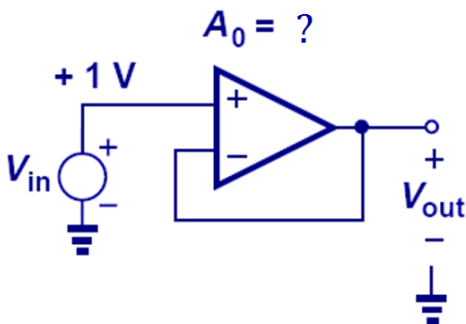
$$\begin{aligned} \text{Power (P)} &= 1.8 \times I_{D1} \\ &= 2 \times 10^{-3} \text{ W} \end{aligned}$$

$$\therefore I_{D1} = 1.11\text{mA}$$

$$\therefore g_m = \sqrt{2 \times (200 \times 10^{-6}) \left(\frac{W}{L}\right) (1.11\text{mA})}$$

$$\therefore \frac{W}{L} = 900 //$$

5. (6%) A unity-gain buffer shown below.  $V_{in+}=1\text{V}$ . What value of  $A_0$  is necessary so that the output voltage is equal to  $0.9999$ ?



Ans:

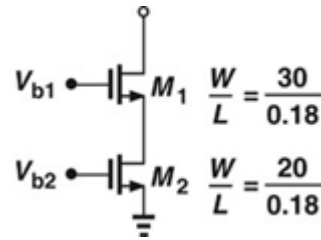
$$V_{out} = A_0 (V_{in} - V_{out}) \frac{V_{out}}{V_{in}} = \frac{A_0}{1 + A_0} = 0.9999$$

$$\Rightarrow 0.9999 + 0.9999A_0 = A_0$$

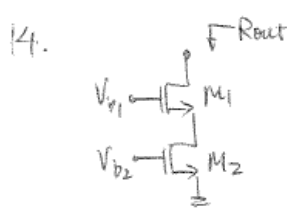
$$\Rightarrow 0.0001A_0 = 0.9999$$

$$\Rightarrow A_0 = 9999 \approx 10000$$

6. (12%) An cascode current source as shown below must be designed for a biasing current of 0.5mA. Assume  $\mu_n C_{ox} = 100 \mu\text{A}/\text{V}^2$ , and  $V_{TH} = 0.4\text{V}$ . (a) (8%) Neglect channel length modulation, compute the required value of  $V_{b2}$ . What is the minimum tolerable of  $V_{b1}$  if M2 must remain saturation? (b) (4%) Assume  $\lambda = 0.1\text{V}^{-1}$ . Calculate the output impedance of the circuit.



Ans:

14.   $(\frac{W}{L})_1 = 30/0.18$   $(\frac{W}{L})_2 = 20/0.18$   
 $I_{BIAS} = 0.5\text{mA}$   
 $\mu_n C_{ox} = 100 \frac{\mu\text{A}}{\text{V}^2}$   $V_{TH} = 0.4\text{V}$

$$(a) I_{D2} = I_{BIAS} = \frac{1}{2} \mu_n C_{ox} \left(\frac{W}{L}\right)_2 (V_{D2} - V_{TH})^2$$

$$\Rightarrow V_{D2} = \sqrt{\frac{2 I_{BIAS}}{\mu_n C_{ox} \left(\frac{W}{L}\right)_2}} + V_{TH}$$

$$= \sqrt{\frac{2(0.5\text{mA})}{(100 \frac{\mu\text{A}}{\text{V}^2})(\frac{20}{0.18})}} + 0.4\text{V} \approx 0.7\text{V}$$

M2 operates in saturation as long as  $V_{GS2} - V_{TH} \leq V_{DS2} \Rightarrow V_{DS2} \geq 0.3\text{V}$ .  
 Observe that  $V_{GS1} = V_{b1} - V_{DS2}$

$$I_{D1} = I_{BIAS} = \frac{1}{2} \mu_n C_{ox} \left(\frac{W}{L}\right)_1 (V_{b1} - V_{DS2} - V_{TH})^2$$

$$\Rightarrow V_{b1} \geq \sqrt{\frac{2 I_{BIAS}}{\mu_n C_{ox} \left(\frac{W}{L}\right)_1}} + 0.4\text{V} + 0.3\text{V}$$

$$\approx \sqrt{\frac{2(0.5\text{mA})}{(100 \frac{\mu\text{A}}{\text{V}^2})(\frac{30}{0.18})}} + 0.7\text{V} \approx 0.95\text{V}$$

$\therefore$  Minimum  $V_{b1} = 0.95\text{V}$ .

$$(b) R_{out} = (1 + g_{m1} r_{o2}) r_{o1} + r_{o2}$$

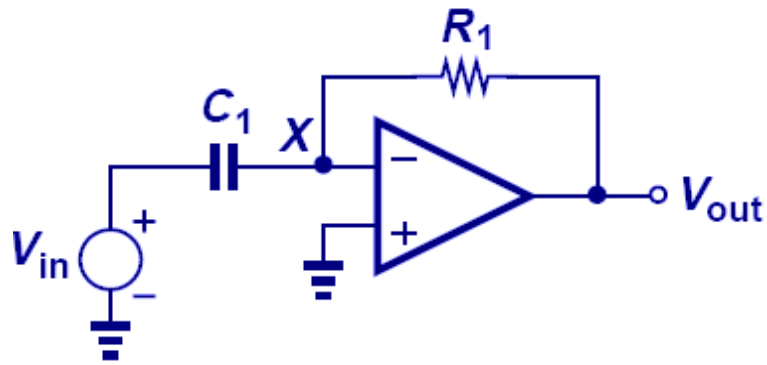
$$= \left(1 + \sqrt{2 \mu_n C_{ox} \left(\frac{W}{L}\right)_1 I_{BIAS}} \cdot \frac{1}{\lambda I_{BIAS}}\right) \cdot \frac{1}{\lambda I_{BIAS}} + \frac{1}{\lambda I_{BIAS}}$$

$$= \left[1 + \sqrt{2 \left(100 \frac{\mu\text{A}}{\text{V}^2}\right) \left(\frac{30}{0.18}\right) (0.5\text{mA})} \cdot \frac{1}{(0.1)(0.5\text{mA})}\right] \cdot \frac{1}{(0.1)(0.5\text{mA})}$$

$$+ \frac{1}{(0.1)(0.5\text{mA})}$$

$$\approx 1.67\text{M}\Omega$$

7. (6%) A differentiator is shown below. Please find the transfer function.

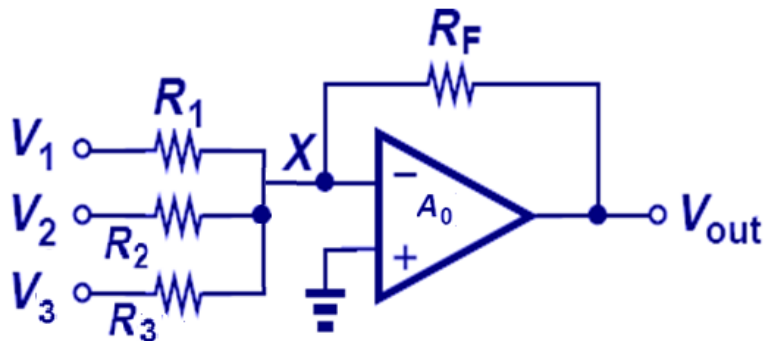


Ans:

$$\frac{V_{in} - V_X}{\frac{1}{C_1 s}} = \frac{V_X - V_{out}}{R_1} \quad V_X = \frac{V_{out}}{-A_0}$$

$$\frac{V_{out}}{V_{in}} = \frac{-R_1 C_1 s}{1 + \frac{1}{A_0} + \frac{R_1 C_1 s}{A_0}}$$

8. (6%) Find the output voltage of the following circuit in terms of  $V_1$ ,  $V_2$ ,  $V_3$ ,  $R_1$ ,  $R_2$ ,  $R_3$  and  $R_F$ .



Ans:

$$\frac{V_1}{R_1} + \frac{V_2}{R_2} + \frac{V_3}{R_3} = \frac{-V_{out}}{R_F}$$

$$V_{out} = -R_F \left( \frac{V_1}{R_1} + \frac{V_2}{R_2} + \frac{V_3}{R_3} \right)$$

9. (6%) An inverting amplifier must provide an input impedance of approximately  $10\text{k}\Omega$  and a nominal gain of 4. If the op amp exhibits an open-loop gain of 1000 and output impedance of  $1\text{k}\Omega$ , determine the

gain error. 
$$\varepsilon = 1 - \frac{A_0 - \frac{R_{out}}{R_1}}{1 + \frac{R_{out}}{R_2} + A_0 + \frac{R_1}{R_2}}$$

Ans:

$$\left| \frac{V_{out}}{V_{in}} \right| = \frac{R_1}{R_2} = 4 \Rightarrow R_{in} \approx R_2 = 10\text{K}\Omega$$

$$R_1 = 4R_2 = 40\text{K}\Omega$$

$$\varepsilon = 1 - \frac{A_0 - \frac{R_{out}}{R_1}}{1 + \frac{R_{out}}{R_2} + A_0 + \frac{R_1}{R_2}} = 0.51\%$$

10. (4%) The integrator of Fig. 8.51 must provide a pole at no higher than 2 Hz. If the values of  $R_1$  and  $C_1$  are limited to  $5\text{ k}\Omega$  and  $50\text{ nF}$ , respectively, determine the required gain of the op amp.

$$S_p = \frac{-1}{2\pi(A_0 + 1)RC}$$

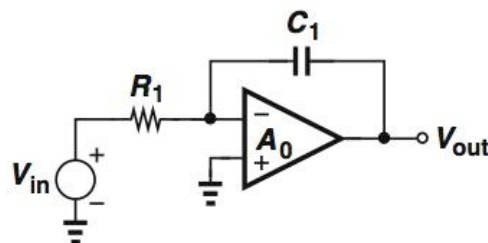
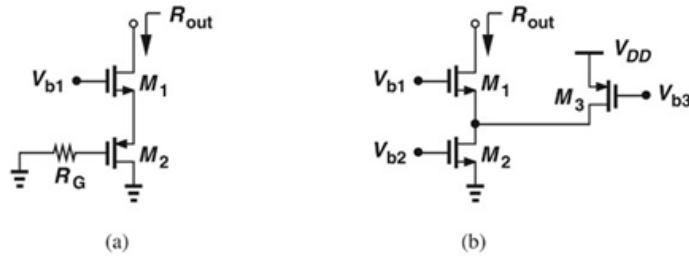


Figure 8.51

Ans:

$$S_p = \frac{-1}{2\pi(A_0 + 1)RC} \leq -2\text{Hz} \Rightarrow 2\pi(A_0 + 1)(5\text{K})(50\text{nF}) \geq 2 \Rightarrow A_0 \geq 1273$$

11. (8%) Determine the output impedance of following two circuits. Assume all transistors operate at saturation and  $g_m r_o \gg 1$ .

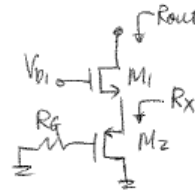


Ans:

19. (a)  $R_x$  is the input impedance of a common-gate configuration:



"Looking into" the source of  $M_2$ ,



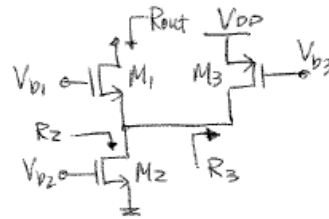
$$R_x = \frac{1}{g_{m2}} \parallel r_{o2}$$

$$\therefore R_{out} = g_{m1} r_{o1} R_x = g_{m1} r_{o1} \left( \frac{1}{g_{m2}} \parallel r_{o2} \right)$$

(b) From observation,

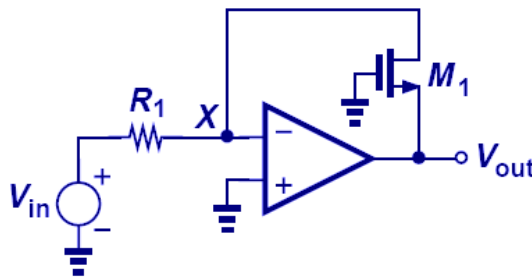
$\rightarrow R_3 = r_{o3}$  ( $\because V_{sg} = 0$  in AC)

$\rightarrow R_2 = r_{o2}$  ( $\because V_{sg} = 0$  in AC)



$$\therefore R_{out} = g_{m1} r_{o1} (R_2 \parallel R_3) = g_{m1} r_{o1} (r_{o2} \parallel r_{o3})$$

12. (6%) Please find the output voltage of the following square root amplifier.



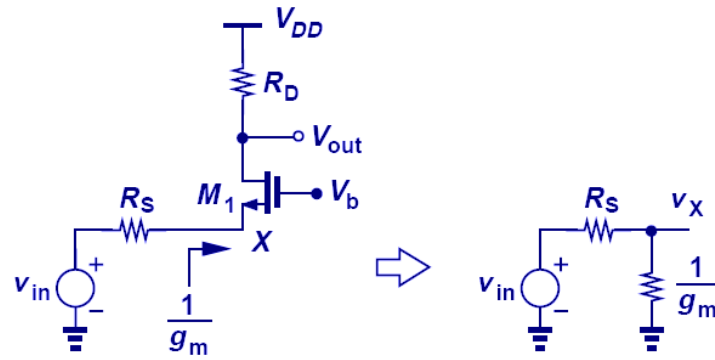
Ans:

$$\frac{V_{in}}{R_1} = \frac{1}{2} \mu_n C_{ox} \frac{W}{L} (V_{GS} - V_{TH})^2$$

$$V_{out} = - \sqrt{\frac{2V_{in}}{\mu_n C_{ox} \frac{W}{L} R_1}} - V_{TH}$$

$$(V_{GS} = -V_{out})$$

13. (6%) Please find the voltage gain of the following Common gate stage with source resistance.

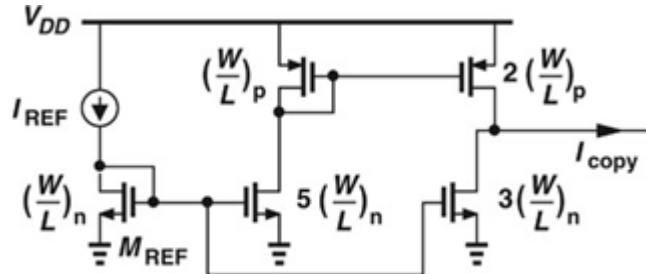


Ans:

$$v_X = \frac{1}{\frac{1}{g_m} + R_S} v_{in} = \frac{1}{1 + g_m R_S} v_{in}$$

$$\frac{v_{out}}{v_{in}} = \frac{v_{out}}{v_X} \frac{v_X}{v_{in}} = \frac{g_m R_D}{1 + g_m R_S} = \frac{R_D}{\frac{1}{g_m} + R_S}$$

14. (6%) Calculate  $I_{copy}$  of the following circuit. Assume all of the transistors operate in saturation.



Ans:

(b)

$$V_{GS, REF} = V_{GS, 1} : I_{D1} = 5 I_{REF}$$

$$V_{GS, 3} = V_{GS, 4} : I_{D4} = 2 I_{D3} = 2 I_{D1} = 10 I_{REF}$$

$$V_{GS, REF} = V_{GS, 2} : I_{D2} = 3 I_{REF}$$

$$\therefore I_{copy} = I_{D4} - I_{D2} = 7 I_{REF}$$